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## ABSTRACT

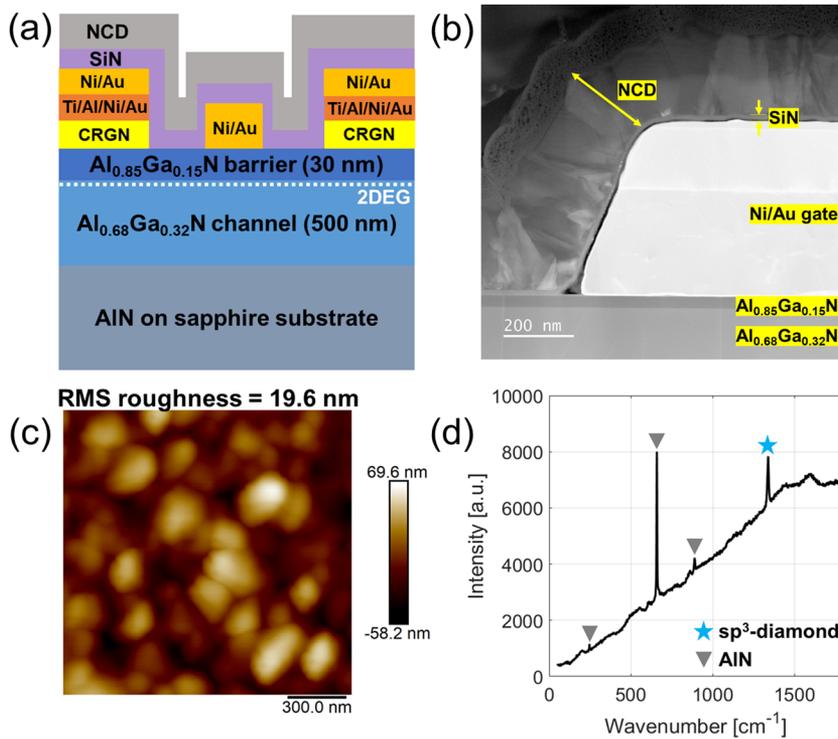
We report back-end-of-line growth of nanocrystalline diamond (NCD) on ultrawide bandgap (UWBG) high Al content aluminum gallium nitride (AlGa<sub>x</sub>N) channel high electron mobility transistors for thermal management. A thin (~15 nm) silicon nitride (SiN<sub>x</sub>) interlayer was deposited to protect the device surface before performing a low temperature (500 °C) NCD growth process in an attempt to protect the gates on these fully fabricated devices. Notably, atomic force microscopy showed that the maximum lateral grain size exceeded 300 nm even though the film thickness was ~250 nm. Comparing electrical (DC) performance before and after NCD growth, the gate leakage increased by ~10<sup>2</sup> after NCD growth. Despite the lower NCD growth temperature, intermixing of the Ni and Au was observed in the Schottky gate metal stack; however, we believe there is another mechanism, possibly hydrogen-related, that is responsible for the measured increase in gate leakage. Regarding thermal management, the device-level thermal resistance (quantified using the average gate temperature rise measured by thermoreflectance imaging) was reduced by 29% through the incorporation of the top-side diamond film. Using time-domain thermoreflectance, the thermal conductivity of the ~250 nm thick NCD film was measured to be 45 ± 25 W m<sup>-1</sup> K<sup>-1</sup>. This is expected to be at least 5× greater than the thermal conductivity of the thin disordered AlGa<sub>x</sub>N alloy. There could also be a coupled electrothermal component contributing to the reduced temperature rise from electric field spreading and consequent heat spreading. This study demonstrates a promising first step toward device-level thermal management of high power UWBG Al-rich AlGa<sub>x</sub>N devices.

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## INTRODUCTION

Ultrawide bandgap (UWBG) semiconductors, such as Al<sub>x</sub>Ga<sub>1-x</sub>N, AlN, β-Ga<sub>2</sub>O<sub>3</sub>, BN, GeO<sub>2</sub>, and diamond, are receiving significant interest and investment in the device research community to realize the next generation of radio frequency (RF) and power electronics.<sup>1,2</sup> UWBG semiconductor device technologies offer the potential for increased radiation tolerance, higher

temperature operation, higher voltage blocking capabilities, and higher power output. Al<sub>x</sub>Ga<sub>1-x</sub>N-based semiconductor devices are an enticing option that benefits from the natural transition of the research, development, and infrastructure of GaN crystal growth, processing, and device fabrication. For lateral devices, this includes transitioning from GaN channel high electron mobility transistors (HEMTs) to Al<sub>x</sub>Ga<sub>1-x</sub>N channel HEMTs,<sup>3,4</sup> for which the development of low contact resistance Ohmic contacts has been



**FIG. 1.** (a) Cross-sectional schematic of the AlGa channel HEMT. (b) Cross-sectional MAADF image of the HEMT with diamond. (c) AFM and (d) Raman of the diamond film.

a significant hurdle until recent demonstrations of reverse-graded nitride regrown contacts.<sup>5–7</sup>

With shrinking device footprints and increasing power demands, an inevitable barrier to widespread adoption and reliability is device self-heating. Overcoming this thermal challenge for GaN-based devices has been extensively studied for years, and this research is ongoing.<sup>8</sup> This is expected to become even more challenging for Al<sub>x</sub>Ga<sub>1-x</sub>N due to its lower thermal conductivity, resulting from disordered alloy scattering.<sup>9,10</sup> As such, it is imperative to consider and incorporate thermal management solutions during the earlier stages of device design and development. For GaN HEMTs, top-side diamond integration has been shown to be an effective method for near-junction thermal management.<sup>11</sup> Accordingly, in this study, we demonstrate back-end-of-line (BEOL) low temperature (500 °C) nanocrystalline diamond (NCD) growth on high Al-content Al<sub>x</sub>Ga<sub>1-x</sub>N ( $x = 0.68$ ) channel HEMTs for top-side thermal management [Fig. 1(a)].

## EXPERIMENTAL METHODS

Metal-organic chemical vapor deposition (MOCVD) was used to grow the HEMT epitaxial layers on AlN/sapphire templates [Fig. 1(a)]. These include a 3.4 μm thick AlN buffer, a 500 nm thick unintentionally doped (UID) Al<sub>0.68</sub>Ga<sub>0.32</sub>N channel, and a 30 nm thick Al<sub>0.85</sub>Ga<sub>0.15</sub>N barrier (Si-doped,  $6 \times 10^{18} \text{ cm}^{-3}$ ). Standard contact lithography was used to fabricate the HEMTs. An W layer was deposited, and footprints for ohmic contact regrowth were opened. Compositional reverse graded (CRGN) Ohmic regrowth<sup>12</sup> consisted of (i) a 10 nm thick Al<sub>0.85</sub>Ga<sub>0.15</sub>N layer (Si-doped,

$6 \times 10^{18} \text{ cm}^{-3}$ ), (ii) a 100 nm thick n+ (Si-doped,  $2\text{--}12 \times 10^{19} \text{ cm}^{-3}$ ) compositionally reverse graded Al<sub>x</sub>Ga<sub>1-x</sub>N layer ( $x = 85\%$  down to  $x = 14\%$ ), and (iii) a 30 nm thick Al<sub>0.14</sub>Ga<sub>0.86</sub>N layer (Si-doped,  $1.2 \times 10^{20} \text{ cm}^{-3}$ ) sequentially grown using MOCVD. The access region was revealed by removing the ohmic regrowth and mask using BCl<sub>3</sub>/Cl<sub>2</sub>-based inductively coupled plasma etching and wet etching. Ohmic contacts were formed via e-beam evaporation of Ti/Al/Ni/Au (25/100/15/50 nm) followed by rapid thermal annealing (700 °C, 30 s, N<sub>2</sub>). Finally, the gate metal (Ni/Au, 20/450 nm) was deposited via e-beam evaporation on both the gate regions and over the Ohmic contacts. The devices had a gate length ( $L_G$ ) of 3 μm, a gate width ( $W_G$ ) of 660 μm, and gate-source ( $L_{GS}$ ) and gate-drain ( $L_{GD}$ ) spacings of 3.5 μm. From circular transmission line method (CTLTM) measurements, the specific contact resistivity ( $\rho_c$ ) and sheet resistance ( $R_{sh}$ ) were measured to be  $6.7 \times 10^{-4} \Omega \text{ cm}^2$  and 6.3 kΩ/sq, respectively.

Following fabrication, a 15 nm thick plasma-enhanced CVD silicon nitride (SiN<sub>x</sub>) layer was deposited at 300 °C as a protective interlayer for aluminum gallium nitride (AlGaN) prior to diamond growth. Subsequently, a  $\approx 0.25 \mu\text{m}$  thick NCD cap was grown via microwave plasma CVD at 500 °C after the AlGaN surface was seeded with detonation nanodiamond particles via an ultrasonication process.<sup>13</sup> The total NCD growth duration was  $\approx 9$  h due to reduced growth rates at lower growth temperatures. The NCD and SiN<sub>x</sub> interlayer were etched via O<sub>2</sub> and SF<sub>6</sub> plasma, respectively, from the metal pads for electrical probing.

Surface roughness and lateral grain size of the NCD film were measured using a Bruker atomic force microscope (AFM). Raman spectroscopy was performed to qualitatively assess the crystalline

quality of the NCD using a Thermo Scientific DXR3xi Raman spectrometer. For the Raman measurements, a 532 nm laser was used with a 100 $\times$  objective and a 25  $\mu\text{m}$  confocal hole. The Raman spectrum was acquired via averaging 100 scans taken with an acquisition rate of 8 Hz and a laser power of 5 mW. Because the energy of the 532 nm laser is sub-bandgap for the semiconductors in the device epitaxial layers (NCD, SiN<sub>x</sub>, AlGaN, and AlN) and the sapphire substrate, laser heating was assumed to be negligible. A Nion Ultra-STEM 200X scanning transmission electron microscope (STEM) with energy dispersive x-ray spectroscopy (EDS) capability was used for cross-sectional imaging and elemental analysis of the device. DC electrical characteristics of the HEMTs were measured using a Keithley 4200A-SCS parameter analyzer.

To measure the operating temperature of the uncapped and NCD-capped AlGaN HEMTs, we elected to use thermoreflectance imaging, a method that relies on the temperature dependence of the reflectance of the device surface. The thermoreflectance system used (TMX Scientific T<sup>o</sup>Imager) is optimized for use with near-UV and visible wavelengths (365–700 nm). Therefore, we used this method to probe the Au-coated gate electrode, which has been demonstrated extensively for estimating peak temperature rise in lateral transistors.<sup>14–23</sup> For the device thermal measurements, we used a probing wavelength of 530 nm, a 100 $\times$  objective, and a device pulse-width of 100 ms, a time-scale that has been shown to be sufficient for lateral AlGaN transistors to reach a quasi-steady state condition.<sup>22</sup>

The thermal conductivity of the NCD film was measured using time-domain thermoreflectance (TDTR) on a witness sample (500  $\mu\text{m}$  thick Si substrate) that underwent both the SiN<sub>x</sub> deposition and NCD growth. For sample preparation, a metal transducer (80 nm thick Al) was deposited via e-beam evaporation after a solvent clean (acetone/isopropyl alcohol). The TDTR measurements were performed in a two-tint configuration<sup>24</sup> using a pulsed Ti:Sapphire laser with a pulse width of 150 fs, a repetition rate of 80 MHz, a central wavelength of 808 nm, and a full width at half maximum (FWHM) of 13 nm. The laser is split into two beam paths (pump and probe) with a half-wave plate and a polarizing beam-splitting cube. The pump provides periodic heating to the sample, which is modulated at 8.4 MHz with an electro-optic modulator. The probe pulses are time-delayed relative to the pulses of the pump with a linear delay stage, which provides up to 5.5 ns of delay. The probe and pump beams are recombined with a dichroic mirror and are concentrically focused on the sample surface, which produces  $1/e^2$

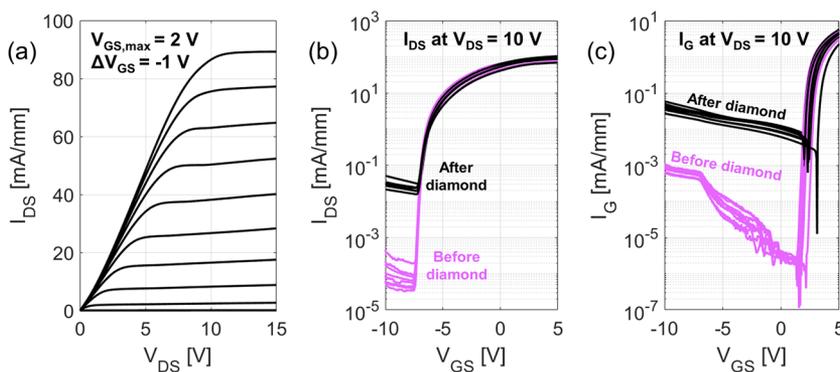
diameters of 12 and 18  $\mu\text{m}$ , respectively. The reflected probe light is detected by a photodetector connected to a lock-in amplifier, which is synchronized to the modulation frequency. The reflected signal is recorded as a function of the delay time between the pump and probe pulses.

To extract thermal properties, we analyze the ratio of the in-phase and out-of-phase lock-in signals using a thermal model,<sup>25</sup> where parameters of interest are obtained via least-squares optimization. We model the sample as a four-layer stack: (1) a nominally 80 nm thick Al transducer, (2) a 260 nm thick NCD, (3) a 13.4 nm thick SiN<sub>x</sub> interlayer, and (4) a 500  $\mu\text{m}$  thick silicon substrate. The Al transducer thickness and thermal conductivity—measured from ps ultrasonic measurements<sup>26</sup> and four-point probe measurements on a witness sample from the Al transducer deposition—are  $81 \pm 3$  nm and  $149 \pm 5$  Wm<sup>-1</sup> K<sup>-1</sup>, respectively. Additional TDTR measurements on a Si substrate and a SiN<sub>x</sub>-on-Si sample were performed to help determine a Si thermal conductivity ( $130 \pm 9$  W m<sup>-1</sup> K<sup>-1</sup>) and an effective SiN<sub>x</sub> thermal conductivity ( $0.73 \pm 0.09$  W m<sup>-1</sup> K<sup>-1</sup>). In this model, the thermal interface resistances are lumped into an effective thermal conductivity of the SiN<sub>x</sub> interlayer in order to reduce the number of fitting parameters. The volumetric heat capacities for each material are assumed from the literature (2.42, 1.78, 1.9, and 1.65 MJ m<sup>-3</sup> K<sup>-1</sup> for the Al, diamond, SiN<sub>x</sub>, and Si, respectively<sup>27–30</sup>). Using this model, we fit for the thermal conductivity of the NCD film. The Al/NCD thermal boundary conductance is also treated as a free parameter and is found to be  $\sim 94$  MW m<sup>-2</sup> K<sup>-1</sup>.

## RESULTS AND DISCUSSION

NCD film thickness and columnar structure are shown in the cross-sectional medium angle annular dark field (MAADF) image in Fig. 1(b). From AFM [Fig. 1(c)], the root-mean-square (rms) surface roughness was measured to be 19.6 nm with lateral grain sizes exceeding 300 nm. This is noteworthy considering the diamond film thickness is on the order of 250 nm. Raman measurements [Fig. 1(d)] confirmed the high crystal quality of the diamond film due to the sharp high-intensity sp<sup>3</sup>-bonded diamond Raman peak.<sup>31</sup>

Figure 2(a) shows the DC output characteristics of the diamond-capped AlGaN channel HEMT. Despite exposure to 9 hours of H<sub>2</sub> plasma during CVD diamond growth at 500 °C as



**FIG. 2.** (a) DC output characteristics of the diamond-capped HEMT. (b) and (c) DC transfer characteristics of the HEMTs before and after diamond growth.

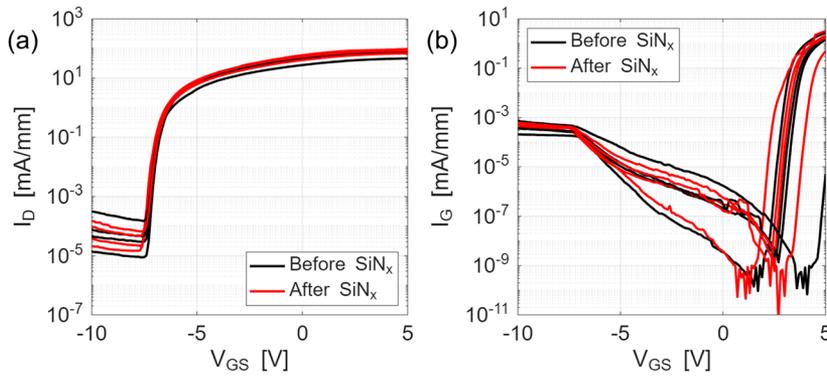


FIG. 3. DC transfer characteristics of (a) drain and (b) gate current of a reference AlGaIn channel HEMT before and after deposition of a thin PECVD SiN<sub>x</sub> film.

a BEOL process, the HEMTs were still functional, demonstrating gate control and an  $I_{DS,max}$  of  $\approx 90$  mA/mm. The DC transfer characteristics ( $I_{DS}$ - $V_{GS}$  and  $I_G$ - $V_{GS}$ ) of the HEMTs before and after diamond growth are shown in Figs. 2(b) and 2(c). After diamond growth, off-state leakage significantly increased by about two orders of magnitude, reducing the on/off ratio from  $10^6$  to  $10^4$ , attributable to an increase in gate leakage current, similar to previous reports.<sup>32,33</sup>

For the origin of the increased leakage current, we first verified that the increase in leakage current was not due to the SiN<sub>x</sub> interlayer. Using an uncapped sister sample, we deposited a thin ( $\approx 15$  nm) PECVD SiN<sub>x</sub> film using the same deposition conditions as used when depositing the SiN<sub>x</sub> interlayer before diamond growth. As shown in Fig. 3, there was a negligible change in the DC transfer characteristics before and after deposition of the SiN<sub>x</sub> film (Fig. 3). There have been reports of Ni/Au contact degradation at high temperatures in HEMTs. Ni/Au mixing and Ni migration have been reported for GaN channel HEMTs operated up to 500 °C in vacuum,<sup>34,35</sup> while gate metal reordering has been reported for Al<sub>x</sub>Ga<sub>1-x</sub>N ( $x = 0.7$ ) channel HEMTs operated at 500 °C in air.<sup>36</sup>

EDS was used to assess the elemental composition of the gate electrode of both a reference (uncapped) and a diamond-capped HEMT.

In Figs. 4(a)–4(c), there is a clear distinction between the Ni and Au films in the Schottky gate of the reference HEMT. On the other hand, after NCD growth, the Ni and Au have intermixed, and there is no longer any distinct Ni or Au metal layer observed [Figs. 4(d)–4(f)]. This degradation of the Schottky gate and Au at the metal–semiconductor interface could explain the measured increase in gate leakage.<sup>37,38</sup> However, when we attempted to simulate only the thermal environment during diamond growth by annealing AlGaIn HEMTs with a thin SiN<sub>x</sub> interlayer (vacuum, 500 °C, 6 h), there was no significant or systematic change in the DC transfer characteristics (Fig. 5). We have also annealed a sister sample of AlGaIn HEMTs up to 850 °C in N<sub>2</sub> for 1 h, performed similar cross-sectional EDS analysis as that shown in Fig. 4, and again observed Ni/Au intermixing yet negligible changes in the DC characteristics.<sup>39</sup> Other potential sources of leakage could be hydrogen plasma exposure and/or H-incorporation in the SiN<sub>x</sub> interlayer, AlGaIn barrier layer, and/or Schottky metal–semiconductor interface,<sup>40,41</sup> or a

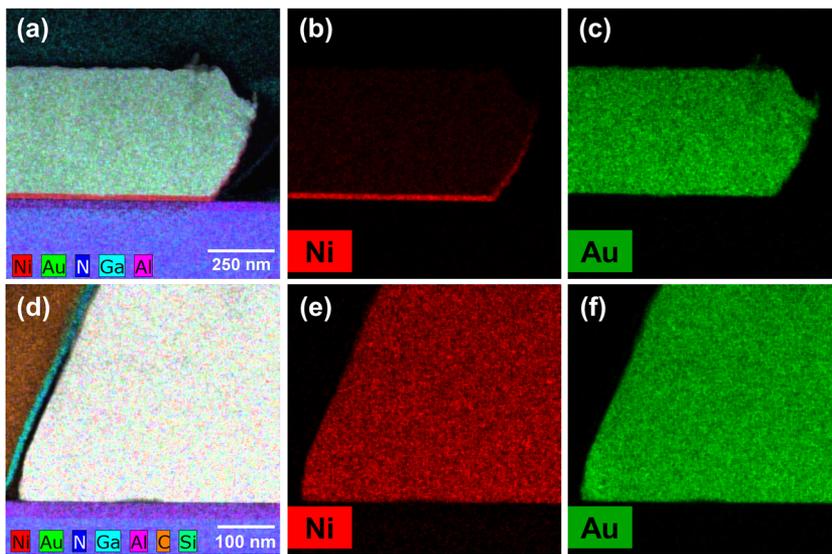
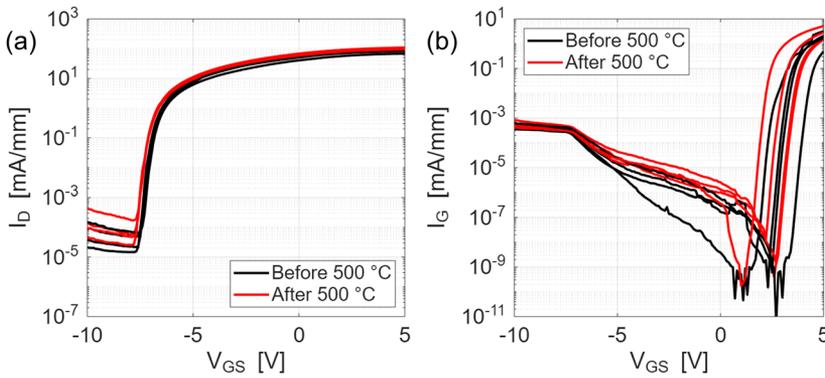


FIG. 4. EDS elemental analysis of the Ni/Au gate electrode of the (a)–(c) uncapped and (d)–(f) diamond-capped HEMTs. (a) and (d) show the elemental analysis with several elements, (b) and (e) show the Ni data, and (c) and (f) show Au data. The slight difference in the appearance of the edge of the gate electrode is due to device processing variability, as the metal lift-off after metal deposition can vary.



**FIG. 5.** DC transfer characteristics of (a) drain and (b) gate current of a reference AlGaIn channel HEMT capped with a thin PECVD Si<sub>x</sub> film only (no diamond) before and after a 6 h anneal at 500 °C in rough vacuum ( $\approx 10$  mT).

combination of the thermal and chemical environment during growth, which is the subject of future work.

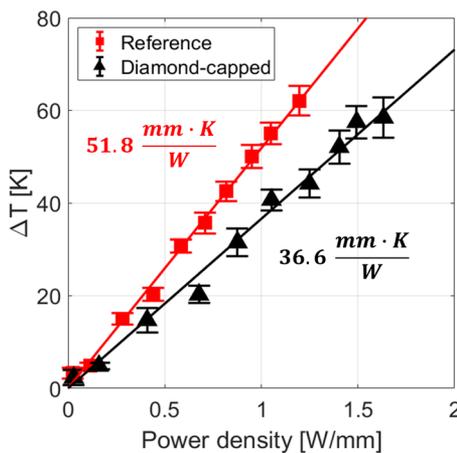
To quantify the effect of the diamond film on the thermal performance of the device, thermoreflectance imaging was performed on both a reference (uncapped, no diamond) and NCD-capped HEMT under open channel conditions ( $V_{GS} = 2$  V) at steady-state ( $\approx 100$  ms bias pulse width<sup>22</sup>). Since our thermoreflectance imaging system has a minimum probing wavelength of 365 nm ( $\approx 3.4$  eV), insufficient for near-bandgap probing of the UWBG AlGaIn channel, we applied this method to probe the Au-coated gate electrode, where an average gate temperature rise of the HEMTs was measured. The gate electrode provides a reasonable estimate of the peak temperature rise of the device due to its proximity to the drain-side edge of the gate, where heat generation is highly localized.<sup>23,42,43</sup> Figure 6 shows that the incorporation of the top-side diamond film, acting as a heat spreader, led to a 29% reduction in device-level thermal resistance: 51.8 mm K/W for the reference HEMT down to 36.6 mm K/W for the diamond-capped HEMT.

Subsequently, the cross-plane (along the NCD film growth direction) thermal conductivity of the NCD film on a witness sample was measured using TDTR (see Experimental Methods section)

to be  $45 \pm 25$  W m<sup>-1</sup> K<sup>-1</sup>. The reported uncertainty accounts for spot-to-spot measurement variability and includes a 5% perturbation in layer thicknesses and thermal conductivities, combined in quadrature. The large uncertainty relative to the measured value can be attributed to low sensitivity to the thermal conductivity of the NCD film as well as a low signal-to-noise ratio at high measurement frequencies. Despite this, the NCD film thermal conductivity is  $>5\times$  higher than the thermal conductivity of thin Al-rich AlGaIn films, which suffer from alloy disorder induced phonon scattering.<sup>9</sup> Moreover, it has been shown that introducing a top-side heat spreading film can also result in electric field spreading.<sup>44-47</sup> This could reduce the electric field concentration at the drain-side edge of the gate and more evenly redistribute the heat generation across the device channel.<sup>48-50</sup> The combination of the NCD thermal conductivity being up to an order of magnitude larger than the AlGaIn channel and the potential field spreading, along with the associated coupled electrothermal effects, both explains and contributes to the measured reduction in gate temperature rise of the diamond-capped AlGaIn HEMT.

**CONCLUSION**

In this study, we demonstrated top-side thermal management of high Al-content Al<sub>x</sub>Ga<sub>1-x</sub>N ( $x = 0.68$ ) channel HEMTs via BEOL diamond growth at 500 °C. Thermoreflectance imaging was used to measure the average gate temperature rise and showed a 29% reduction in device-level thermal resistance due to the incorporation of top-side diamond. Using TDTR, the cross-plane thermal conductivity of the NCD film was measured to be  $45 \pm 25$  W m<sup>-1</sup> K<sup>-1</sup>, which is expected to be at least  $>5\times$  higher than the thin AlGaIn layers with very low thermal conductivity due to disordered alloy scattering. Regarding electrical performance, the OFF-state leakage of the HEMTs increased following diamond growth. While intermixing of the Ni and Au in the Schottky gate was observed via EDS, we believe another mechanism is responsible for the gate leakage, possibly due to H-plasma exposure and H-incorporation in the Si<sub>x</sub> interlayer, AlGaIn barrier, and/or Schottky metal-semiconductor interface. Avenues for future study include (i) investigating electrothermal device performance using novel interlayers,<sup>51</sup> (ii) developing thermally robust gate metallization capable of withstanding BEOL diamond growth, (iii) studying the effect of hydrogen on AlGaIn HEMT performance, and (iv) demonstrating diamond growth before gate



**FIG. 6.** Average temperature rise of the gate electrode of the uncapped (reference) and diamond-capped HEMTs as a function of power density ( $V_{GS} = 2$  V).

metal deposition to allow higher diamond growth temperatures and more readily obtain thicker films and larger lateral grain sizes with higher thermal conductivity.<sup>52,53</sup>

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## AUTHOR DECLARATIONS

### Conflict of Interest

The authors have no conflicts to disclose.

## Author Contributions

**James Spencer Lundh:** Conceptualization (equal); Formal analysis (equal); Investigation (equal); Methodology (equal); Validation (equal); Writing – original draft (lead); Writing – review & editing (lead). **Brianna A. Klein:** Conceptualization (equal); Formal analysis (equal); Investigation (equal); Methodology (equal); Validation (equal); Writing – review & editing (equal). **Tatyana I. Feygelson:** Conceptualization (equal); Formal analysis (equal); Investigation (equal). **Daniel J. Pennachio:** Conceptualization (equal); Formal analysis (equal); Investigation (equal). **Andrew A. Allerman:** Conceptualization (equal); Formal analysis (equal); Investigation (equal). **GlenAsia Gonzalez:** Conceptualization (equal); Formal analysis (equal); Investigation (equal). **Emma G. Rocco:** Conceptualization (equal); Formal analysis (equal); Investigation (equal). **Hannah N. Masten:** Conceptualization (equal); Formal

analysis (equal); Investigation (equal). **Geoffrey M. Foster:** Conceptualization (equal); Formal analysis (equal); Investigation (equal). **Katie R. Gann:** Conceptualization (equal); Formal analysis (equal); Investigation (equal). **Alan G. Jacobs:** Conceptualization (equal); Formal analysis (equal); Investigation (equal). **Andrew M. Armstrong:** Conceptualization (equal); Funding acquisition (equal); Project administration (equal); Resources (equal); Supervision (equal). **Ethan A. Scott:** Formal analysis (equal); Investigation (equal); Methodology (equal). **Patrick E. Hopkins:** Formal analysis (equal); Investigation (equal); Methodology (equal). **Marko J. Tadjer:** Conceptualization (equal); Formal analysis (equal); Investigation (equal); Resources (equal); Supervision (equal); Writing – review & editing (equal). **Bradford B. Pate:** Conceptualization (equal); Funding acquisition (equal); Project administration (equal); Resources (equal); Supervision (equal). **Karl D. Hobart:** Conceptualization (equal); Funding acquisition (equal); Project administration (equal); Resources (equal); Supervision (equal). **Michael A. Mastro:** Conceptualization (equal); Funding acquisition (equal); Project administration (equal); Resources (equal); Supervision (equal).

## DATA AVAILABILITY

The data that support the findings of this study are available within the article.

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