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# Size effects in the thermal conductivity of gallium oxide ( $\beta$ -Ga<sub>2</sub>O<sub>3</sub>) films grown via open-atmosphere annealing of gallium nitride

Chester J. Szwejkowski,<sup>1</sup> Nicole C. Creange,<sup>2</sup> Kai Sun,<sup>3</sup> Ashutosh Giri,<sup>1</sup> Brian F. Donovan,<sup>1</sup> Costel Constantin,<sup>2,a)</sup> and Patrick E. Hopkins<sup>1,b)</sup>

<sup>1</sup>Department of Mechanical and Aerospace Engineering, University of Virginia, Charlottesville, Virginia 22904, USA

<sup>2</sup>Department of Physics and Astronomy, James Madison University, Harrisonburg, Virginia 22807, USA

<sup>3</sup>Department of Materials Science and Engineering, University of Michigan, Ann Arbor, Michigan 48109, USA

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Gallium nitride (GaN) is a widely used semiconductor for high frequency and high power devices due to its unique electrical properties: a wide band gap, high breakdown field, and high electron mobility. However, thermal management has become a limiting factor regarding efficiency, lifetime, and advancement of GaN devices and GaN-based applications. In this work, we study the thermal conductivity of beta-phase gallium oxide ( $\beta$ -Ga<sub>2</sub>O<sub>3</sub>) thin films, a component of typical gate oxides used in such devices. We use time domain thermoreflectance to measure the thermal conductivity of a variety of polycrystalline  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films of different thicknesses grown via open atmosphere annealing of the surfaces of GaN films on sapphire substrates. We show that the measured effective thermal conductivity of these  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films can span 1.5 orders of magnitude, increasing with an increased film thickness, which is indicative of the relatively large intrinsic thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> grown via this technique ( $8.8 \pm 3.4 \text{ W m}^{-1} \text{ K}^{-1}$ ) and large mean free paths compared to typical gate dielectrics commonly used in GaN device contacts. By conducting time domain thermoreflectance (TDTR) measurements with different metal transducers (Al, Au, and Au with a Ti wetting layer), we attribute this variation in effective thermal conductivity to a combination of size effects in the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> film resulting from phonon scattering at the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface and thermal transport across the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface. The measured thermal properties of open atmosphere-grown  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> and its interface with GaN set the stage for thermal engineering of gate contacts in high frequency GaN-based devices. © 2015 AIP Publishing LLC. [<http://dx.doi.org/10.1063/1.4913601>]

## I. INTRODUCTION

As the characteristic times and lengths of devices decrease to scales on the order of the carrier scattering rates and mean free paths, thermal management of material boundaries can become a critical aspect of design.<sup>1–3</sup> In this regime, the energy transport mechanisms that are intrinsic to the materials comprising the device can contribute much less to the overall thermal resistance of the system as compared to the resistances across the individual interfaces. The efficacy of transmitting energy across these solid interfaces can be quantified via the thermal boundary conductance,<sup>4</sup> or Kapitza Conductance,<sup>5</sup> (the inverse of which is the thermal boundary resistance or Kapitza Resistance), and is the constant of proportionality that relates the heat flux to the temperature drop across this interfacial region, mathematically expressed as  $h_K = q/\Delta T$ , where  $h_K$  is the thermal boundary conductance,  $q$  is the thermal flux, and  $\Delta T$  is the interfacial temperature drop.<sup>4</sup> The range of phonon-dominated thermal boundary conductances between solids at room temperature span roughly two orders of magnitude from  $\sim 5$  to  $500 \text{ MW m}^{-2} \text{ K}^{-1}$ , and can be strongly related to the atomic structure and chemistry around the interface.<sup>6</sup> To

put this into perspective, this energy transport pathway can offer the equivalent thermal resistance as roughly 300–3.0 nm of high quality SiO<sub>2</sub>, respectively. Given the wide spread use of thin gate oxides and additional sacrificial layers in electronic nanodevices, the addition of this thermal resistance associated with interfaces can be highly detrimental to device operation and reliability.

Interfacial thermal engineering has emerged as a solution to bottlenecks in development of high power devices.<sup>7</sup> Where the processor industry has hit roadblocks in maintaining Moore's Law from on chip power densities exceeding  $100 \text{ W cm}^{-2}$  (higher than a typical lab hotplate),<sup>7</sup> even greater power densities have been observed in radio frequency (RF) amplifier gallium nitride-based (GaN) devices.<sup>8,9</sup> This increase in power density creates massive hot-spots in GaN active regions, mainly concentrated near the gate contacts, which directly leads to underperformance and eventual failure of these devices. This thermal bottleneck therefore creates a major issue for furthering of GaN-based technologies, such as high-electron-mobility transistors (HEMTs) for high frequency devices, light emitting diodes (LEDs) for energy-efficient illumination, radar technologies (ship-board, airborne, and ground), and high performance space satellites.

Accordingly, engineering of the thermal properties and energy transport mechanisms associated with the GaN gate contacts can elucidate thermal mitigation mechanisms to

<sup>a)</sup>Email: constacx@jmu.edu

<sup>b)</sup>Email: phopkins@virginia.edu

improve GaN performance by reducing Joule heating effects attributed with the thermal resistances at these junctions. In a typical GaN device, such as a MOSFET, the thermal resistances associated with this junction will consist of the metal electrode, a high-dielectric constant (“high- $k$ ”) gate oxide, the GaN channel, and the material interfaces at each of these contacts. It is well known that typical gate oxides can have very low thermal conductivities ( $\sim 1 \text{ W m}^{-1} \text{ K}^{-1}$ ), and can vary greatly depending on the deposition procedure.<sup>10–12</sup> However, the thermal properties of  $\beta\text{-Ga}_2\text{O}_3$ , a common component of gate oxides in high frequency devices (including GaN),<sup>13–15</sup> are relatively unstudied. Furthermore, the effects of film thickness on the thermal properties of this oxide, corresponding thermal boundary conductances at the  $\beta\text{-Ga}_2\text{O}_3$ -contact interfaces, and the interfacial morphology effects on thermal transport have never been experimentally determined, which has imposed a significant roadblock in gate-contact thermal mitigation.

In response, we report on the size effects in the thermal conductivity of beta-phase gallium oxide ( $\beta\text{-Ga}_2\text{O}_3$ ) films grown via annealing (0001) GaN surfaces in open atmosphere. We show that open atmosphere annealing of GaN surfaces can create polycrystalline, phase pure films of  $\beta\text{-Ga}_2\text{O}_3$  with varying thicknesses. The duration of the GaN-anneal also leads to both surface roughness on the  $\beta\text{-Ga}_2\text{O}_3$  and spiking of the  $\beta\text{-Ga}_2\text{O}_3$  phase into the GaN. We measure the thermal conductance of the  $\beta\text{-Ga}_2\text{O}_3$  films and interfaces in adjunction using time domain thermoreflectance (TDTR). From our measurements, we quantify the thermal boundary conductance across the  $\beta\text{-Ga}_2\text{O}_3$ /GaN interface to be in close proximity to the previously reported interface conductance inferred for  $\text{SiO}_2$ /Si interfaces, another common gate oxide/channel interface widely found in several technologies. However, unlike typical gate oxides, we show that the effective thermal conductivity of our polycrystalline  $\beta\text{-Ga}_2\text{O}_3$  can span 1.5 orders of magnitude, increasing with an increased film thickness due to size effects from phonon scattering at the  $\beta\text{-Ga}_2\text{O}_3$ /GaN interface. From this analysis, we determine that the intrinsic thermal conductivity of open atmosphere grown  $\beta\text{-Ga}_2\text{O}_3$  is  $8.8 \pm 3.4 \text{ W m}^{-1} \text{ K}^{-1}$ , much higher than typical amorphous gate oxides. This study demonstrates the promise of  $\beta\text{-Ga}_2\text{O}_3$  grown via open atmosphere anneal of GaN as a potential oxide that can be used to mitigate near-gate hotspots in GaN devices.

## II. GALLIUM OXIDE FABRICATION AND CHEMICAL CHARACTERIZATION

The various gallium oxide films fabricated in this study were developed from commercially available,  $5 \text{ mm} \times 5 \text{ mm}$ , single-side polished GaN films ( $3.4 \mu\text{m}$ ) on sapphire substrates ( $430 \mu\text{m}$ ) obtained from University Wafer. The GaN films have a Wurtzite crystal structure and are unintentionally n-type doped. To ensure a clean surface prior to annealing, the samples were ultrasonicated for 20 min. in acetone, 20 min. in isopropanol, 20 min. in deionized water, and then dried with inert air. Following this cleaning procedure, we annealed the samples in a tube furnace subjected to a wide variety of annealing conditions, adapted and modified

from previous procedures.<sup>16–18</sup> Samples were annealed in 10 min. cycles between  $900\text{--}1050^\circ\text{C}$ . This initiated not only growth of gallium oxide<sup>19,20</sup> but also varying degrees of roughness at both the surface of the gallium oxide and the gallium oxide/GaN interface, as observed previously.<sup>21–23</sup> The surface roughness of the gallium oxide was determined using a combination of atomic force microscopy (AFM, Veeco DI Multimode IIIa) and mechanical profilometry. We also approximated the grain size of the  $\text{Ga}_2\text{O}_3$  layer using AFM images and the linear intercept method to verify that the grain size is larger than the film thickness. The unannealed samples (which were the smoothest) had RMS roughness values ( $R_q$ ) as low as  $0.5 \text{ nm}$ , while the roughest sample had  $R_q$  over  $70 \text{ nm}$  with many intermediate roughnesses in between (c.f., Figs. 1(a)–1(h)). The roughness and compositional variance on the GaN surface where growth was initiated were observed with transmission electron microscopy (TEM) and scanning transmission electron microscopy (STEM). The TEM and STEM images reveal that annealing not only caused growth of a rough oxide layer but also changed the compositional abruptness of the  $\text{Ga}_2\text{O}_3$ /GaN interface. Roughness and “spiking” at the interface can be seen in the TEM and STEM images presented in Figs. 1(i)–1(n). Table I summarizes the  $\text{Ga}_2\text{O}_3$  thicknesses and surface roughnesses determined from the AFM, TEM, and STEM measurements.

The chemistry of the oxide layer was determined using x-ray diffraction (XRD) and x-ray photoelectron spectroscopy (XPS). In Figs. 2(a)–2(d), we present the XRD spectra taken in the range of  $2\theta = 20^\circ\text{--}130^\circ$  as a function of  $R_q$  obtained from a PANalytical X’Pert PRO MPD  $\theta$ - $2\theta$  diffractometer with x-ray radiation of Cu ( $\lambda = 1.54060 \text{ \AA}$  for Cu  $K_\alpha$  peak). The signature GaN peaks are observed at  $34.39(3)^\circ$  (0002),  $72.69(8)^\circ$  (0004), and  $125.89(1)^\circ$  (0006). The Sapphire peaks are observed at  $41.63(1)^\circ$  (0006), and  $90.49(7)^\circ$  (00012). The other peaks observed at  $2\theta = 31.16(6)^\circ$ ,  $38.32(6)^\circ$ , and  $59.02(2)^\circ$  correspond to crystallographic planes of (002), (202), and (113) for  $\beta\text{-Ga}_2\text{O}_3$ . These  $\beta\text{-Ga}_2\text{O}_3$  layers are polycrystalline and form crystallites that have single crystal monoclinic structure, as determined via the AFM, TEM, STEM, and XRD. According to structure factor calculations, the Miller Indices for such monoclinic structures should obey  $h + k = 2n$  with  $n = 1, 2, 3, 4, \dots \infty$ . The  $d$ -spacing for a monoclinic crystal structure is calculated according to

$$\frac{1}{d^2} = \frac{1}{\sin^2(\beta)} \left[ \frac{h^2}{a^2} + \frac{k^2 \sin^2(\beta)}{b^2} + \frac{l^2}{c^2} - \frac{2hl \cos(\beta)}{ac} \right], \quad (1)$$

where  $hkl$  are the Miller Indices,  $abc$  are the unit cell lattice constants, and  $\alpha\beta\gamma$  are the unit cell internal angles. Equation (1) was useful to check the Miller indices for our  $\beta\text{-Ga}_2\text{O}_3$  layers by using well known values for  $a$ ,  $b$ , and  $c$  as found in the literature.<sup>24</sup> With Bragg’s law [i.e.,  $n\lambda = 2d \sin(\theta)$ ], we determined the  $d$  lattice spacings to be  $d_{002} = 2.867(4) \text{ \AA}$ ,  $d_{202} = 2.346(6) \text{ \AA}$ ,  $d_{113} = 1.563(8) \text{ \AA}$ , in excellent agreement with those reported by Lv *et al.* (i.e.,  $d_{002} = 2.82(9) \text{ \AA}$ ,  $d_{202} = 2.34(4) \text{ \AA}$ , and  $d_{113} = 1.53(3) \text{ \AA}$ ).<sup>25</sup> The  $\text{O}_{1s}$  XPS spectra in Fig. 2(e) are presented as a function of surface roughness for our samples with  $R_q = 1.0, 4.9, 9.7$ , and  $12.7 \text{ nm}$ .



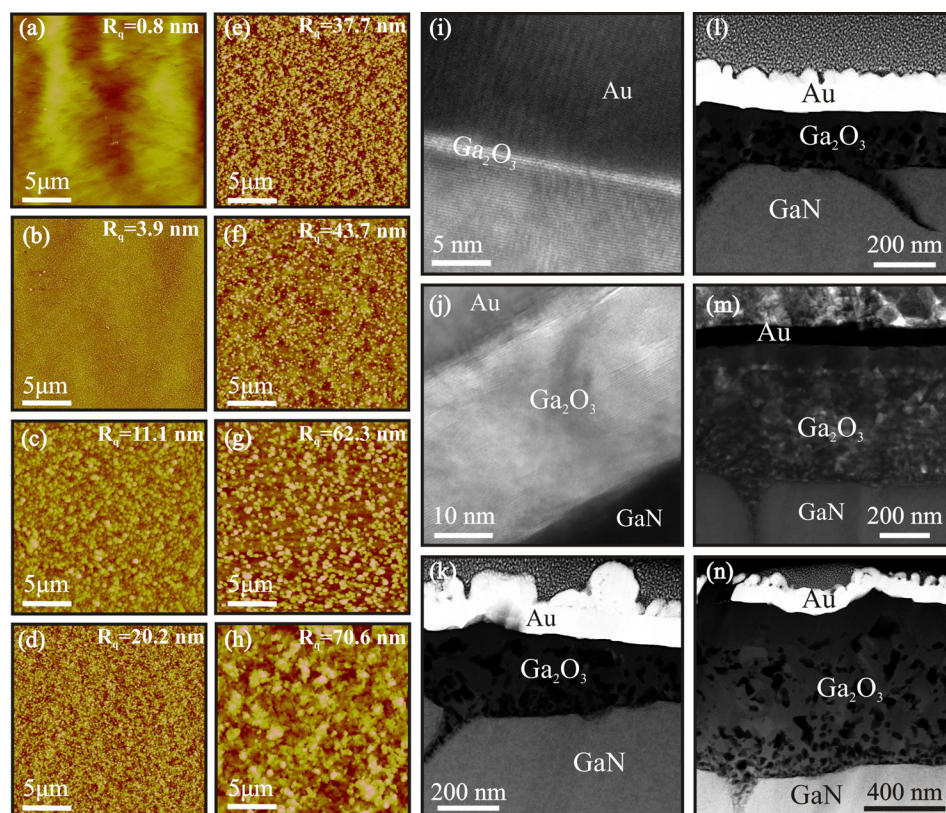


FIG. 1. (a)–(h) Atomic force microscopy images of Ga<sub>2</sub>O<sub>3</sub>-GaN-Sapphire surfaces for  $R_q = 0.8$ –70.6 nm. (i), (j), and (m) Cross-sectional high resolution transmission electron microscopy for sample with  $R_q = 0.9$ –77.2 nm. (k), (l), and (n) High angle annular dark-field images collected in STEM mode for sample with  $R_q = 0.9$ –77.2 nm.

The binding energies of the examined elements were calibrated using  $C_{1s}$  peak (284.6 eV) as a reference. The binding energies for our samples were found to be 534.5 eV ( $R_q = 0.5$  nm), 530.50 eV ( $R_q = 4.9$  nm), 530.34 eV ( $R_q = 9.7$  nm), and 530.15 eV ( $R_q = 12.7$  nm). These  $O_{1s}$  spectra indicate that the as-received sample (i.e., not annealed and with 0.5 nm RMS roughness—blue curve in Fig. 2) contains a much smaller signature of oxygen compared to the annealed samples; this is consistent with typical thicknesses of native Ga<sub>2</sub>O<sub>3</sub> on the GaN surface (i.e., a surface layer of 1–2 nm).<sup>26</sup> It is important to note that as the Ga<sub>2</sub>O<sub>3</sub> layer increases in thickness, the  $O_{1s}$  shifts towards smaller binding energies, consistent with previous XPS studies showing the effect of the Ga<sub>2</sub>O<sub>3</sub> on the GaN spectrum.<sup>27</sup>

We measured the thicknesses of the gallium oxide layer with TEM and STEM, example high-resolution electron

micrographs and high angle annular dark-field images of which are presented in Fig. 1(i)–1(n). The TEM and STEM analysis confirms that the increase in surface roughness measured via AFM is directly correlated to an increase in oxide layer thickness. We relate the thickness of gallium oxide to the roughness via a 3rd order polynomial fit (Fig. 3), and use this calibration for analysis of our TDTR measurements, described in more detail below. The error bars in the roughness represent one standard deviation, based on AFM measurements, which are propagated through our polynomial fit to determine the uncertainty in Ga<sub>2</sub>O<sub>3</sub> thickness.

For TDTR measurements, we electron-beam evaporate thin metal films on the various Ga<sub>2</sub>O<sub>3</sub>/GaN samples using metals similar to those employed in electronic devices: 79 nm Au, 78 nm Au with a 2 nm Ti wetting layer, and 89 nm Al. The film thicknesses were verified using a combination

TABLE I. Three sets of samples were fabricated regarding the metal transducer that was deposited. The roughness of the RMS surface of the samples before transducer deposition ( $R_q$ ) and the thickness of the gallium oxide layer ( $d$ ) are summarized. Uncertainties in roughness represent one standard deviation of the AFM measurements, while uncertainties in thickness are calculated from our model (Fig. 3) propagating the roughness uncertainty.

Transducer $\beta$ -Ga <sub>2</sub> O <sub>3</sub>	Au (79 nm)		Al (89 nm)		Au (78 nm)/Ti (2 nm)	
	$R_q$ (nm)	$d$ (nm)	$R_q$ (nm)	$d$ (nm)	$R_q$ (nm)	$d$ (nm)
	$0.9 \pm 0.2$	$2.2 \pm 0.4$	$0.8 \pm 0.2$	$2.2 \pm 0.4$	$0.8 \pm 0.2$	$2.2 \pm 0.4$
	$6.6 \pm 0.1$	$13.2 \pm 0.7$	$4.0 \pm 0.1$	$6.9 \pm 0.4$	$6.9 \pm 0.5$	$14.0 \pm 2.7$
	$11.6 \pm 0.4$	$31.2 \pm 3.8$	$5.0 \pm 0.7$	$9.1 \pm 3.0$	$13.5 \pm 0.2$	$40.2 \pm 2.0$
	$25.9 \pm 0.2$	$124.3 \pm 2.7$	$10.8 \pm 1.1$	$27.9 \pm 9.1$	$33.8 \pm 1.6$	$199.7 \pm 34.1$
	$45.9 \pm 2.8$	$345.7 \pm 74.9$	$14.5 \pm 1.0$	$45.3 \pm 11.0$	$43.2 \pm 0.1$	$310.0 \pm 2.8$
	$60.2 \pm 0.5$	$559.0 \pm 18.0$	$19.4 \pm 0.1$	$74.6 \pm 1.2$	$77.2 \pm 1.7$	$864.0 \pm 64.8$
	...	...	$30.2 \pm 0.4$	$163.3 \pm 7.8$	...	...
	...	...	$41.6 \pm 2.1$	$289.8 \pm 52.6$	...	...
	...	...	$65.6 \pm 2.4$	$651.0 \pm 83.2$	...	...

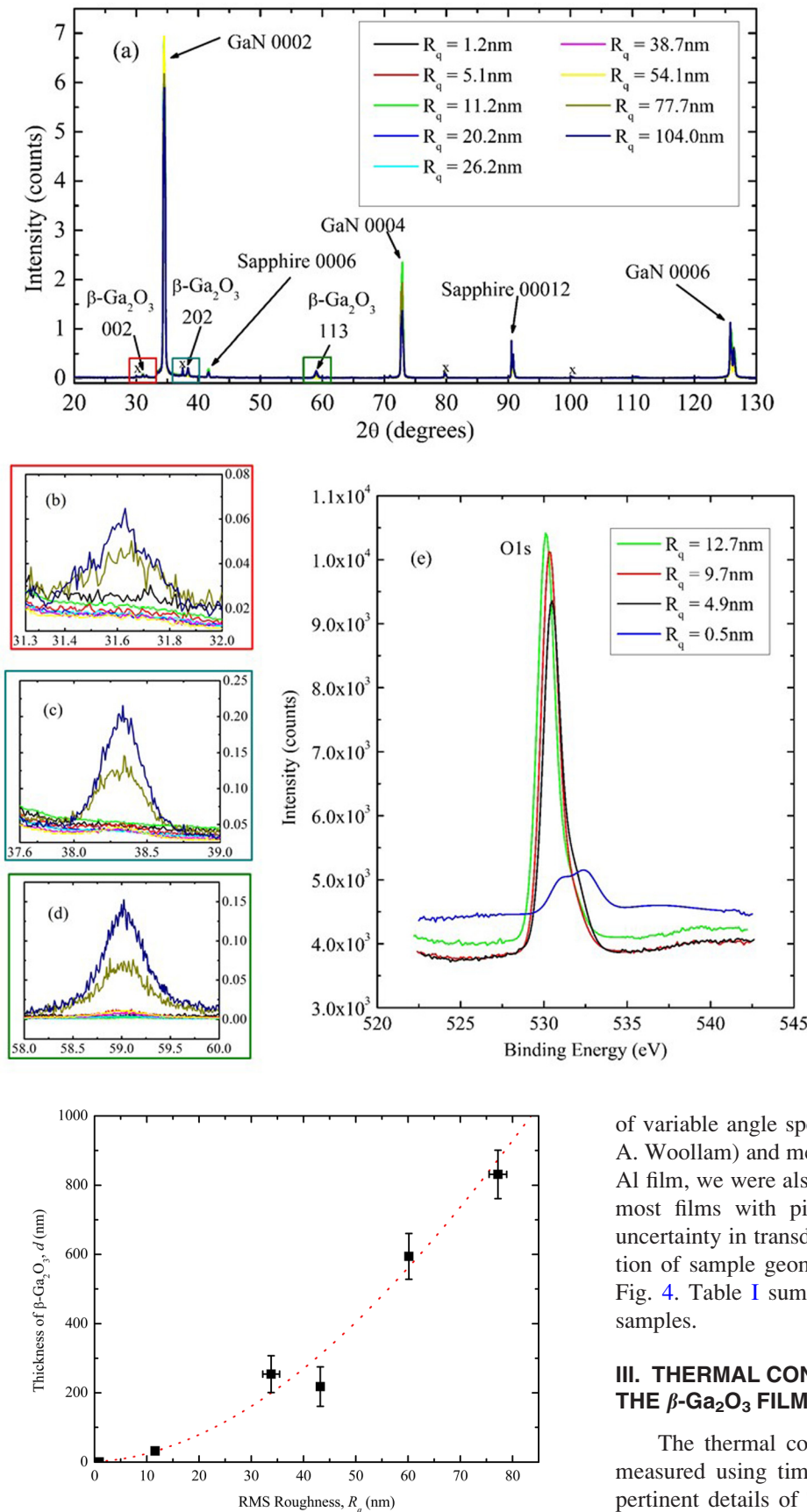


FIG. 3.  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> thickness measured via TEM vs. surface roughness measured via AFM. The relationship is modeled by the red dotted line with a third order polynomial equation:  $d = -0.0004(R_q)^3 + 0.1667(R_q)^2 + 0.6869(R_q) + 1.5$ . This was found to be a statistically sound correlation ( $R^2 = 0.975$ ,  $t = 12.6$ ,  $t_{2=0.005} = 4.60$ ).

FIG. 2. XRD-XPS. (a) X-ray diffraction ( $\theta$ - $2\theta$ ) of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>-GaN-Sapphire (0001) thin films as a function of surface roughness root mean square ( $R_q$ ) for  $R_q = 0.9$ –104.0 nm. (b)–(d) Scaled up figures for the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> signature peaks (i.e.,  $2\theta = 31.6^\circ$ ,  $38.3^\circ$ ,  $59.0^\circ$ ). (e) X-ray photoemission spectroscopy for oxygen O<sub>1s</sub> peak observed at ~530 eV.

of variable angle spectroscopic ellipsometry (VASE from J. A. Woollam) and mechanical profilometry. In the case of the Al film, we were also able to confirm the film thicknesses of most films with picosecond acoustics.<sup>28,29</sup> We report an uncertainty in transducer film thickness of 3 nm. An illustration of sample geometries studied in this work is shown in Fig. 4. Table I summarizes the information for each set of samples.

### III. THERMAL CONDUCTIVITY MEASUREMENTS OF THE $\beta$ -Ga<sub>2</sub>O<sub>3</sub> FILMS

The thermal conductivities of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films were measured using time domain thermoreflectance (TDTR);<sup>30</sup> pertinent details of TDTR and corresponding data analyses can be found in the literature.<sup>31–33</sup> To briefly summarize, our TDTR experiment is a pump-probe technique utilizing sub-picosecond laser pulses that are split into two paths: the pump and probe. The pump pulses are absorbed by the sample and cause a change in the surface temperature on the

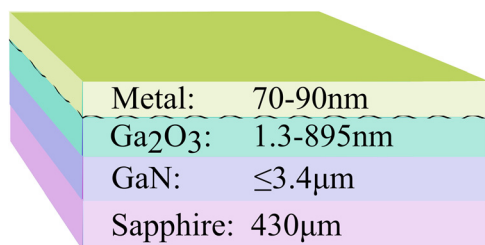


FIG. 4. Illustration of sample geometries studied in this work. The fabrication of our samples includes two stages: the gallium oxide growth and then the metal film deposition. Starting with the commercially available GaN on sapphire, the oxide was grown via open atmosphere annealing for 10 min cycles at temperatures between 900–1050°C; longer anneals increased the roughness at the oxide surface (indicated by the textured line above the oxide layer). Various metal films were then electron-beam evaporated on top including aluminum, gold, and gold with a titanium adhesion layer.

metal film. This surface temperature decays based on the thermal properties of the materials underneath (in our case, the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> film, the GaN film, the Al<sub>2</sub>O<sub>3</sub> substrate, and the associated interfaces) and the temporal change in temperature is subsequently monitored as a function of time via the change in thermorefectance of the probe pulse.<sup>34–36</sup>

In our specific experiments, we use the sub-picosecond pulses emitted from an 80 MHz Ti:Sapphire oscillator with a central wavelength of 800 nm ( $\sim 10.5$  nm bandwidth) as the basis of our pump-probe experiments. The pump path is modulated at 8.8 MHz, doubled to 400 nm, and focused onto the surface of the metal transducer layer while the thermorefectivity of the probe path is monitored at the pump frequency with a time-delay of up to 5.5 ns after the initial heating event. The radii of the pump and probe paths are 25  $\mu$ m and 6.5  $\mu$ m, respectively, so the heat flow is nearly entirely dominated by cross plane conduction (normal to the interfaces). We used TDTR to characterize the thermal conductance through the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films and associated interfaces in the three sets of GaN samples (each set is referring to a different metal film transducer). Each set had between six and eight samples with different surface roughnesses based on the annealing conditions, as summarized in Table I. Finally, at least three TDTR scans were performed on each sample to ensure repeatability in our thermal measurements.

The method we use for our data analysis and extracting the effective thermal conductivity of our  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films is described in detail in the literature.<sup>31–33</sup> In short, we fit a multilayer, diffusive thermal model that accounts for the periodic heating of the laser pulses to our TDTR measurements. The inputs to our model analysis require knowledge of the heat capacity, thermal conductivity, and thermal boundary conductance associated with each layer of the system. We used literature values for the heat capacity of GaN (Ref. 37) and  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> (Ref. 38) and for the heat capacities and thermal conductivities of Al (Ref. 39) and Au (Ref. 40). At a modulation frequency of 8.8 MHz, the thermal penetration depth in these samples is at most  $\sim 2$   $\mu$ m. Thus, we are not sensitive to the thermal properties of the sapphire substrate or thermal boundary conductance across the GaN/sapphire interface. For the as-received samples, we determined across the transducer/GaN interface using a two-layer model

(transducer/GaN), treating the nanometer of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> native oxide as part of the transducer/GaN interface. This measured value for the thermal conductivity of the GaN film was used as a known parameter for analyzing the remaining annealed samples with the same metal transducers. It is important to note that when the thicknesses of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films get above a few 10's of nm, the thermal resistance from the metal to the GaN is dominated by the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> and its associated interfaces, and we are relatively insensitive to the thermal conductivity of the GaN.<sup>41</sup> Another assumption in our thermal analyses of the metal/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN samples is that we fix the thermal boundary conductance measured across the transducer/GaN interface in our control (native) samples to be equal to that of the transducer/Ga<sub>2</sub>O<sub>3</sub> interface in the annealed samples. For the annealed samples, we used a three-layer model (transducer/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN) to determine the thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>, where we only fit the thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> layer. In this analysis, we assumed that the thermal boundary conductance at the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface was very large (i.e., we assumed that this interface offers negligible resistance), so that the measured thermal conductivities of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> layer from the TDTR measurements are in fact “effective” thermal conductivities that are also influenced by the presence of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface. Therefore, the only parameter that we vary to fit our thermal model to our TDTR data is the thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>. To simplify our analysis, we ignore grain boundary scattering since the grain sizes are larger than the film thicknesses, making film thickness the limiting dimension. As discussed later, through analyses of the effective thermal conductivities as a function of film thickness, we resolve the intrinsic thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> by considering both thermal boundary conductance across the transducer/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub> interface<sup>42</sup> and phonon scattering at the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface.

Example TDTR data and the corresponding model fit are shown in Fig. 5. We note that there are slight differences in curvature between our best-fit thermal model and the measured data, which we attribute to not fitting for the thermal boundary conductance at the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface. As we previously mentioned, we analyze our data based on only fitting one parameter in our thermal model, the thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>; note, this also exemplifies the power in our procedure as we impose minimal assumptions in our analysis to determine the effective thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>, and we can use the identical analysis procedure for all samples in this work, regardless of the thicknesses of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> and varying sensitivities to the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface conductance. However, because of this approach, the uncertainties in our reported values are larger than those reported in typical TDTR measurements, discussed below.

The uncertainty in our measurements factors in the repeatability of the measurements and uncertainty in transducer and Ga<sub>2</sub>O<sub>3</sub> film thicknesses. From this, the mean uncertainty in our TDTR measurements is  $\sim 15\%$ , and up to  $\sim 25\%$  for the roughest samples. We note that for  $R_q$  above  $\sim 50$  nm, there are long timescale oscillations, as seen in the right inset of Fig. 5. The long-period oscillations observed in



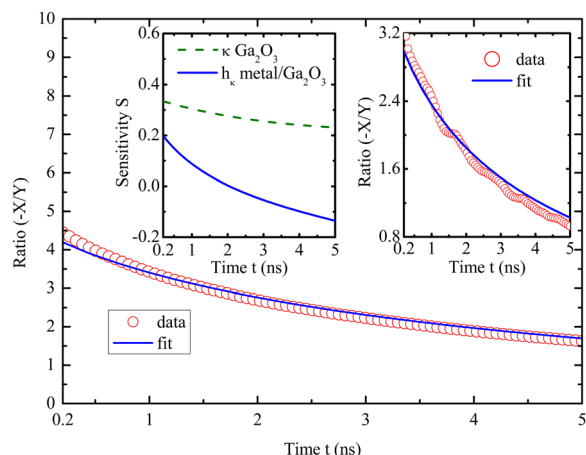


FIG. 5. Thermoreflectance response versus pump-probe delay time. All x-axes are from 0.2 to 5 ns, corresponding to the time regime used to fit for the thermal properties. The large plot and the right inset show the ratio of real and imaginary components of the thermoreflectance response from the lock-in amplifier ( $-X/Y$ ) as a function of time, and feature the data collected with TDTR (red circles) and the model fit (solid blue line). The large figure is from a relatively smooth sample ( $R_q = 6.6$  nm), while the inset is from one of our roughest sample ( $R_q = 60$  nm). Note that there are slight differences in curvature between our best-fit thermal model and the measured data, which we attribute to not fitting for the thermal boundary conductance at the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface. As discussed in detail in the text, we analyze our data based on only fitting one parameter in our thermal model, the thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>. Because of this approach, the uncertainties in our reported values are larger than those reported in typical TDTR measurements. In the case of the rough samples (right inset), the long-period oscillations observed could be indicative of thermoelastic effects on the surface of the sample, which are not accounted for in TDTR analyses. Hence, the uncertainty in determining the thermal conductivity for these samples are relatively large, and highlights the limits of using TDTR to measure thermal properties of rough samples. The left inset depicts the sensitivity on the y-axis, showing that from 0.2 to 5 ns, we remain most sensitive to the thermal conductivity of Ga<sub>2</sub>O<sub>3</sub> (dashed green line), while less sensitive to the thermal boundary conductance at the transducer/Ga<sub>2</sub>O<sub>3</sub> interface (solid blue line) for a rough sample ( $R_q = 60$  nm).

these rough samples could be indicative of thermoelastic wave effects on the surface of these samples, which are not accounted for in our TDTR analyses to extract the thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films. Hence, the uncertainties in determining the thermal conductivities of the thicker films with large roughnesses substantially increase. This highlights the limits of using TDTR at these wavelengths to measure thermal properties of rough samples, as once the surface roughness increases above  $\sim 50$  nm, non-thermal artifacts along with diffusive scattering can skew traditional TDTR analyses. However, we note that even in the roughest sample, we are still sensitive to the thermal conductivity of the Ga<sub>2</sub>O<sub>3</sub> film, as exemplified in the left inset of Fig. 5 (here, sensitivity to a parameter is reflected by a large relative magnitude over the pump-probe delay time). To this point, we note that for our thickest and most rough samples, our reported thermal conductivities have larger uncertainties up to  $\sim 25\%$  or  $\pm 2.0$  W m<sup>-1</sup> K<sup>-1</sup>.

#### IV. RESULTS AND DISCUSSION

The effective thermal conductivities of the gallium oxide films are plotted as a function of film thickness in Fig. 6. Our measurements follow typical thickness-

dependent trends reported in the literature for thermal conductivities of other dielectric films both amorphous and crystalline.<sup>3,11,42-45</sup> In the case of the thermal conductivity of the varying thicknesses of amorphous or disordered films, these trends are indicative of the thermal boundary conductance across the film/substrate interface that is included in the measurements of the effective thermal conductivities of the films. However, unlike the thermal conductivities of the amorphous SiO<sub>2</sub> and SiN<sub>x</sub> films, the thermal conductivity of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> increases up to thicknesses of several hundred nanometers, approaching 1  $\mu$ m, with a continued increase in measured thermal conductivity even in the case where our TDTR measurements are insensitive to the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN thermal boundary conductance. This is indicative of the higher intrinsic thermal conductivity of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> and longer phonon mean free paths compared to the amorphous materials resulting in traditional size effects in the thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>;<sup>3,43</sup> this is not surprising due to the polycrystalline nature of our  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> compared to the amorphous SiO<sub>2</sub> and SiN<sub>x</sub> films, which—due to the lack of periodicity in their atomic structures—will have intrinsically smaller vibrational mean free paths. The range in measured effective thermal conductivities of the gallium oxide films span 1.5 orders of magnitude; 0.34 W m<sup>-1</sup> K<sup>-1</sup> for a film thickness of 12.5 nm up to 8.85 W m<sup>-1</sup> K<sup>-1</sup> for a film thickness of 895 nm. The trends are conserved for all three types of samples regarding the metal transducer indicating that there is no appreciable dependence on the transducer.

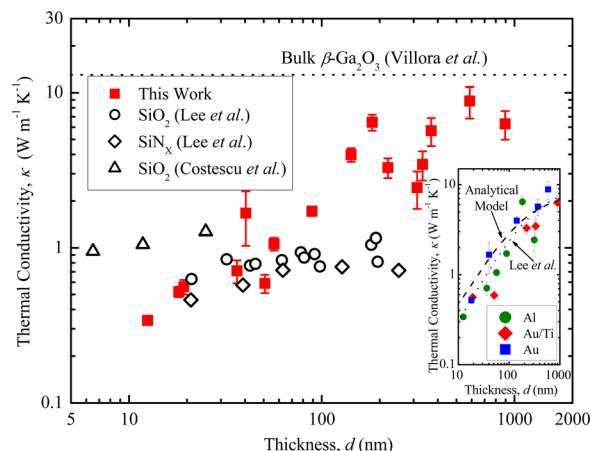


FIG. 6. Measured thermal conductivity as a function of film thickness for our  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films compared to other thin film dielectrics. The thermal conductivity of gallium oxide (filled squares) increases with increased film thickness and approaches the previously reported bulk thermal conductivity (dotted line).<sup>49</sup> This follows the same trend as other dielectric films reported by Lee and Cahill<sup>42</sup> (open circles: SiO<sub>2</sub>; diamonds: SiN<sub>x</sub>) and Costescu *et al.*<sup>11</sup> (open triangles: SiO<sub>2</sub>) and is attributed to boundary scattering. (Inset) Measured thermal conductivity vs. thickness of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films with the different metal transducers used (filled circles: aluminum; filled diamonds: gold with titanium wetting layer; filled squares: gold), suggesting that the thermal resistance at the transducer/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub> is negligible; from this, we conclude that the primary mechanism driving the size effects in the measured thermal conductivities of these films is the thermal resistance associated with the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface. The black dotted line is the model used to resolve the thermal boundary conductance across the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface, adapted from Lee *et al.*<sup>42</sup> The black dashed line is the analytical model based on phonon thermal conductivity using Umklapp and boundary scattering to account for size effects in thermal conductivity.

From the data in Fig. 6, we can determine the intrinsic thermal conductivity of our  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films through two different modeling approaches that consider different origins of the measured thickness dependence in the effective thermal conductivities of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films. The first approach assumes that the reduction in the measured effective thermal conductivity is due to the thermal boundary conductance at the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface, which is included in the measured resistance of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> layer during TDTR analysis. The second approach assumes that the reduction in the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> is due to phonon-boundary scattering leading to size effects in the thermal conductivity. We note that most likely neither approach accurately describes the phonon thermophysics over the entire range of sample thicknesses, but by considering both scenarios, we can improve our accuracy our reported values for the intrinsic thermal conductivity of these  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> samples.

Our first approach to analyze the data in Fig. 6 assumes that the thickness dependence in the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> thermal conductivity is an artifact of the thermal boundary conductance across the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface being included in the measured effective thermal conductivity extracted from our TDTR measurements. Using the expression presented by Lee and Cahill,<sup>42</sup> the intrinsic thermal conductivity of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> can be derived from our data via

$$\kappa_m = \frac{\kappa_i}{1 + \frac{\kappa_i}{h_K d}}, \quad (2)$$

where  $\kappa_m$  is the measured thermal conductivity,  $\kappa_i$  is the intrinsic thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>,  $h_K$  is the thermal boundary conductance, and  $d$  is the thickness of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>. Equation (2) treats the metal/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub> thermal conductance, the thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> film, and the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN thermal conductance as resistors in series. However, we rule out the inclusion of the resistance across the metal/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub> in calculations of Eq. (2) due to the following two reasons: (i) in our TDTR analysis of the thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>, we only fit the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> thermal conductivity, as we are inherently insensitive to the metal/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub> boundary conductance due to the relatively larger resistance of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> film; and (ii) as shown in the inset of Fig. 6, we do not show any systematic, noticeable dependence in the measured thermal conductivity of the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> for the samples with different metallic transducers. Since we have previously shown that the thermal boundary conductance across these metal films/native  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interfaces can vary by a factor of five depending on the metal film,<sup>41</sup> we conclude that this metal/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub> is not contributing to the thermal processes measured in our TDTR experiments. Therefore, the value for thermal boundary conductance in Eq. (2) is representative of the thermal transport across the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface. We fit Eq. (2) to our data to extract the thermal conductivity of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> and the thermal boundary conductance across the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface (fit shown as dotted line in inset of Fig. 6). From this, we determine a  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN thermal boundary conductance

of  $31.2 \pm 8.1 \text{ MW m}^{-2} \text{ K}^{-1}$  and the corresponding intrinsic thermal conductivity of our of open atmosphere-grown  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> of  $9.7 \pm 2.5 \text{ W m}^{-1} \text{ K}^{-1}$ .

The above analysis attributes the reduction in effective thermal conductivity to thermal boundary conductance (suggesting the thermal conductivity of the film is independent of film thickness and the boundary conductance is a byproduct of the measurement). This assumption is clearly not valid for the thicker films where our TDTR measurements are insensitive to the thermal resistance associated with the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface. Therefore, we analyze our data using the second approach in which we model our results with a boundary scattering term in the Kinetic Theory-based expression for the thermal conductivity of phonons, given by

$$\kappa = \frac{1}{3} \sum_{j=1}^3 \int_0^{\omega_{max,j}} \hbar \omega \mathcal{D}_j(\omega) \frac{\partial f_{BE}}{\partial T} v_j^2(\omega) \left( \frac{1}{\tau_i} + \frac{v_j(\omega)}{d} \right)^{-1} d\omega, \quad (3)$$

where  $\mathcal{D}$  is the density of states,  $\partial f_{BE}/\partial T$  is the temperature derivative of the Bose-Einstein distribution function,  $v$  is the phonon group velocity,  $\tau_i$  is the Umklapp scattering time, and  $d$  is the film thickness. The subscript  $j$  denotes the branch in the phonon dispersion for the summation. We use a sine-type phonon dispersion for the three acoustic branches of Ga<sub>2</sub>O<sub>3</sub> and literature values for frequencies at the Brillouin Zone edge ( $\omega_{max,j} = 3.60 \text{ THz}$ ,  $4.14 \text{ THz}$ , and  $4.44 \text{ THz}$ )<sup>46</sup> and the lattice constant ( $a = 5.80 \text{ \AA}$ )<sup>46</sup>

$$\omega(\mathbf{k}) = \omega_{max} \sin \frac{\mathbf{k}a}{2}, \quad (4)$$

or, solving for  $\mathbf{k}$ ,

$$\mathbf{k}(\omega) = \frac{2}{a} \sin^{-1} \frac{\omega}{\omega_{max}}. \quad (5)$$

This allows us to write the velocity and density of states as functions of frequency

$$v(\omega) = \frac{\omega_{max}a}{2} \sqrt{1 - \left( \frac{\omega}{\omega_{max}} \right)^2}, \quad (6)$$

$$\mathcal{D}(\omega) = \frac{4 \left[ \sin^{-1} \frac{\omega}{\omega_{max}} \right]^2}{\pi \omega_{max} a^3 \sqrt{1 - \left( \frac{\omega}{\omega_{max}} \right)^2}}. \quad (7)$$

Using Eq. (3), the trend in the predicted thermal conductivity vs. thickness is similar to that predicted via Eq. (2), as seen by the black dashed line in the inset of Figure 6, but it provides a slightly different result for the intrinsic thermal conductivity of our of open atmosphere-grown Ga<sub>2</sub>O<sub>3</sub> ( $\kappa = 8.0 \pm 2.3 \text{ W m}^{-1} \text{ K}^{-1}$ ), because the thickness-dependencies typical in size effects of the thermal conductivity of films are not necessarily one-to-one correlated with the thermal boundary conductance across solid interfaces.<sup>47,48</sup> Stated differently, the thermal boundary conductance cannot fully account for the size effects in thermal conductivity. Future studies on size effects in the thermal conductivity and



thermal boundary conductance across solid interfaces that are focused on more ideal, traditionally studied nanomaterial systems should be pursued to elucidate the relationship between phonon-boundary scattering, its effects on the reduction in thermal conductivity, and its contribution to thermal transport across solid/solid interfaces. Furthermore, for applications of our material systems, the concern lies in the total thermal resistance that the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> film adds to heat flow from the metal contact into the GaN layer.

Taking an average of the results from both approaches to model the thickness dependence in the thermal conductivity of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>, we therefore report that the intrinsic thermal conductivity of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> grown via open-atmosphere annealing of GaN is  $8.8 \pm 3.4 \text{ W m}^{-1} \text{ K}^{-1}$ . This thermal conductivity is slightly lower than a previous measurement of the thermal conductivity of bulk, single crystalline  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> ( $\sim 13 \text{ W m}^{-1} \text{ K}^{-1}$ —black dotted line in Fig. 6),<sup>49,50</sup> and roughly half the value of the thermal conductivity of typical GaN HFET component AlGaIn ( $16.6 \text{ W m}^{-1} \text{ K}^{-1}$ ).<sup>51</sup> Given the polycrystalline nature of our  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films, this reduction in thermal conductivity relative to the single crystalline value reported in Ref. 49 is not surprising. Similarly, the defects in our films arising from our method of synthesis and clearly observed in our TEM images in Fig. 1 would also lead to a reduction in thermal conductivity compared to higher quality, single crystalline  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>. Although the intrinsic thermal conductivity of our  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> is nearly an order of magnitude larger than the other typical gate insulators shown in Fig. 6 (amorphous SiO<sub>2</sub> and SiN<sub>x</sub>), boundary effects are pronounced enough that for typical gate oxide thicknesses, the effective thermal conductivity is reduced to similar values as these gate dielectric materials.

We attribute the relatively large variation in measured thermal conductivity (both from the analytical models and among the samples with different metal transducers) at larger  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> thicknesses to fluctuations in roughness as a consequence of the relatively simple growth method used to produce  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>. The samples were annealed in a tube furnace open to the atmosphere until the desired roughness was achieved. As shown in Figure 1, this can produce a violent interface between the substrate and the growth, resulting in inconsistent interfacial properties. Therefore, some of our specific samples are not ideally modeled with the simplified analytical approach applied to the data in Fig. 6. However, with our rigorous uncertainty analysis, this model gives appropriate insight into the thermal properties of open-atmosphere grown  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>.

The opportunity for thermal benefits in GaN devices arises in manipulating the thermal boundary conductance across the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface. As previously mentioned, using Eq. (2) and the previous-discussed assumptions associated with this, we determined  $h_K$  across this interface as  $31.2 \pm 8.1 \text{ MW m}^{-2} \text{ K}^{-1}$ . This is on the same order as the room temperature thermal boundary conductances reported for SiO<sub>2</sub>/Si interfaces ( $h_K = 50 \text{ MW m}^{-2} \text{ K}^{-1}$ )<sup>42</sup> and dislocation dense GaSb/GaAs interfaces grown epitaxially ( $h_K = 10\text{--}20 \text{ MW m}^{-2} \text{ K}^{-1}$ ).<sup>52</sup> Our TEM and STEM analyses shown in Fig. 1 indicate the “imperfect” nature of the boundary between the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> and GaN, which can lead to large

reductions in thermal boundary conductance.<sup>6</sup> Given this relatively low conductance (large resistance) associated with this interface compared to the intrinsic thermal conduction mechanisms in bulk  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>, the opportunity exists to engineer this interface and thereby increase the overall thermal conduction across a metal/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN junction.

The possibility of increasing the thermal conductance across metal/ $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN junctions has tremendous implications for thermal mitigation of GaN-based devices by engineering hot spots around gate regions. Beta-phase Ga<sub>2</sub>O<sub>3</sub> is easily grown on GaN via thermal oxidation, and it has many of the necessary electronic characteristics to be used as a gate oxide: low density of states at the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface,<sup>53</sup> high breakdown field,<sup>53</sup> high dielectric constant,<sup>53</sup> and wide band gap.<sup>54</sup> Although, the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN valence and conduction band offsets are low: 1.4 eV and 0.1 eV, respectively,<sup>55</sup> compared to 4.4 eV and 3.4 eV for SiO<sub>2</sub>/Si,<sup>56</sup> which could lead to increased leakage current. Furthermore,  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> is very chemically stable, even in concentrated acids,<sup>57</sup> which could be problematic or promotional for chemical etching procedures depending on what the end goal is. Thus, further chemical and electronic research is necessary to realize the full potential of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> as a gate dielectric. However, this issue is outside the scope of this study; our focus is thermal characterization. Our thermal measurements of open atmosphere-grown  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> demonstrate the intrinsically larger thermal conductivity and mean free paths compared to typical amorphous gate dielectrics, indicating the possibility for increased thermal spreading of heat from localized hot spots at gate/channel contacts compared to typical dielectric and passivation layers. This makes annealing of GaN to form surface layers of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> a promising candidate for gate dielectrics and other surface passivation layers in next generation GaN devices.

## V. SUMMARY

Our work reports on the size effects of the thermal conductivity of beta-phase gallium oxide ( $\beta$ -Ga<sub>2</sub>O<sub>3</sub>) thin films, a component of typical gate oxides used in such devices. We use time domain thermoreflectance to measure the thermal conductivity of a variety of polycrystalline  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> films of different thicknesses grown via open atmosphere annealing of GaN surfaces. We confirm that the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> grown from annealing the GaN surface is phase-pure, and varies in both surface roughness and diffusion into the GaN based on annealing time. The effective thermal conductivity of  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> can span 1.5 orders of magnitude, increasing with an increased film thickness, which is indicative of the relatively large intrinsic thermal conductivity of bulk  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> ( $8.8 \pm 3.4 \text{ W m}^{-1} \text{ K}^{-1}$ ) and large mean free paths compared to typical gate dielectrics commonly used in GaN device contacts. By conducting TDTR measurements with different metal transducers (Al, Au, and Au with a Ti wetting layer), we attribute this variation in effective thermal conductivity to a combination of size effects in the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> film resulting from phonon scattering at the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface and thermal transport across the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface. From our measurements and assuming a series resistor model, we

quantify the thermal boundary conductance across the  $\beta$ -Ga<sub>2</sub>O<sub>3</sub>/GaN interface as  $31.2 \pm 8.1 \text{ MW m}^{-2} \text{ K}^{-1}$ , in the range of typical thermal boundary conductances previously observed non-metal/non-metal interfaces. The measured thermal properties of open atmosphere-grown  $\beta$ -Ga<sub>2</sub>O<sub>3</sub> and its interface with GaN set the stage for thermal engineering of gate contacts in high frequency GaN-based devices.

## ACKNOWLEDGMENTS

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